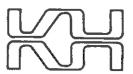
SOLID STATE WIDE RANGE

BAND-PASS FILTER

MODEL 3103(R) SERIAL NO. 930

-24 Sb/OCTAVE

OPERATING AND MAINTENANCE MANUAL



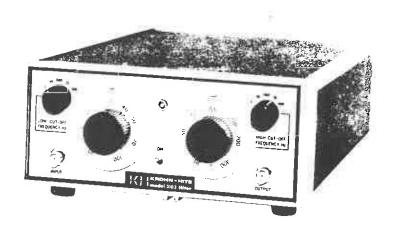
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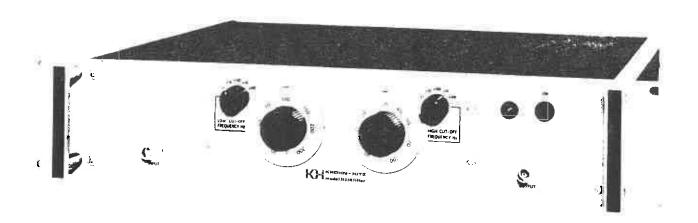
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Model 3103



Model 3103R

Figure 1. Model 3103 and 3103R Filters

GENERAL DESCRIPTION

1.1 INTRODUCTION

The Model 3103(R), illustrated in Figure 1, is a solid state variable electronic band-pass Filter with a low cutoff frequency range adjustable continuously from 10 Hz to 1 MHz and a high cutoff range from 30 Hz to 3 MHz. The pass-band gain is unity (0 db), with attenuation rate of 24 db per octave outside the pass-band, and a maximum attenuation of 80 db. Maximum input signal amplitude is 3 volts rms and output hum and noise is less than 150 microvolts.

As shown in the Simplified Schematic Diagram, Figure 2, the Filter consists basically of an input amplifier, a variable low-pass section (high cutoff frequency), and a variable high-pass (low cutoff frequency) section all connected in series. Both cutoff frequencies are tuned capacitively in decade steps by the band multiplier switch, and continuously within each decade by the frequency dial which varies four cascaded resistor-filter elements. A response switch S1 selects the desired filter characteristics.

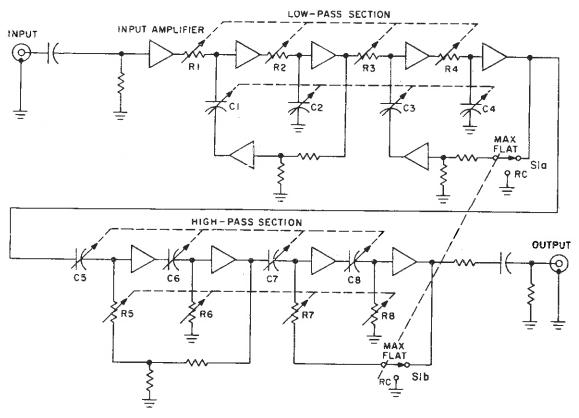


Figure 2. Simplified Schematic Diagram

1.2 SPECIFICATIONS

Frequency range: Low-cutoff frequency independently adjustable from 10 Hz to 1 MHz in five bands.

Band	Multiplier	Frequency (Hz)
1	1	10 - 100
2	10	100 - 1,000
3	100	1,000 - 10,000
4	1 K	10,000 - 100,000
5	10K	100,000 - 1,000,000

High-cutoff frequency independently adjustable from 30 Hz to 3 MHz in five bands.

Multiplier	Frequency (Hz)
1	30 - 300
10	300 - 3,000
100	3,000 - 30,000
1,000	30,000 - 300,000
10,000	300,000 = 3,000,000
	1 10 100 1,000

Frequency dials: Separate low-cutoff and high-cutoff dials are individually calibrated with single logarithmic scales reading directly in Hz, from 9.5 to 105, and from 28 to 310.

Cutoff frequency calibration accuracy: ±5% with RESPONSE switch in MAXimum FLAT (Butterworth) position; less accurate in RC position. Relative to mid-band level, the Filter output is down 3 db at cutoff in maximum flat position, and approximately 13 db in RC position.

Bandwidth: Continuously variable within the cutoff frequency limits of 10 Hz and 3 MHz.

Attenuation slope: Nominal 24 db per octave.

Maximum attenuation: Greater than 80 db. See Section 5.2.

Pass Band Gain: Zero db ± 1/2 db.

Frequency Response: Standard response is 4th order Butterworth, maximally flat. A

RESPONSE switch on rear of chassis converts to simple RC response optimum for transient-free performance.

Input characteristics:

Maximum Input Amplitude: 3 volts rms. 2.5 volts at 3 MHz.

Impedance: 100k ohms in parallel with 50 pf. Maximum DC Component: 200 volts.

Output characteristics:

Maximum Voltage: 3 volts rms, 2.5 volts at 3 MHz.

Maximum Current: 10 milliamperes rms.

Hum and noise: Less than 150 microvolts. Internal Impedance: Approximately 50 ohms.

Floating (ungrounded) Operation: A chassis GROUND switch is provided on rear of chassis to disconnect signal ground from chassis ground.

Front panel controls:

LOW CUTOFF FREQUENCY dial and multiplier switch.

HIGH CUTOFF FREQUENCY dial and multiplier switch.

Power-ON switch.

Terminals: Front panel and rear of chassis, one BNC connector for INPUT, one for OUT-PUT.

Power requirements: 105-125 or 210-250 volts, single phase, 50-400 Hz, 15 watts.

Dimensions and weights: Standard bench Model 3103, 85/8" wide, 31/2" high, 15" deep, 11 lbs net, 22 lbs shipping.

Rack-mounting Model 3103R, 19" wide, 31/2" high, 15" deep, 13 lbs net, 24 lbs shipping.

Note: for detailed definition of specifications refer to Section 5.2.

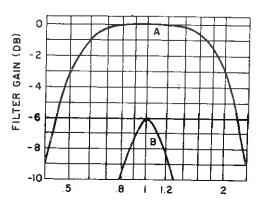


Figure 3. Normalized Filter Response

BANDWIDTH ADJUSTMENT

The flexibility of adjustment of bandwidth is illustrated in Figure 3. Band-pass operation in the MAXimally FLAT or Butterworth mode for two different bandwidths is illustrated by curves A and B. Curve B shows the minimum pass-band width obtained by setting the two cutoff frequencies equal. In this condition the insertion loss is 6 db, and the -3 db cutoff frequencies occur at 0.8 and 1.25 times the mid-band frequency. The minimum pass-band for a 0 db $\pm 1/2$ db passband gain is shown by curve A with the cutoffs set at 0.5 and 2 times the mid-band frequency.

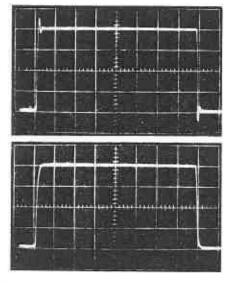


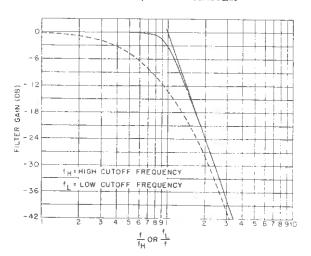
Figure 4. Response to 10 kHz Square Wave with Cutoffs at 10 Hz and 1 MHz. (A) Butterworth, (B) Simple RC

TRANSIENT RESPONSE

The frequency response characteristic of this Filter closely approximates a fourth-order Butterworth with maximal flatness, ideal for filtering in the frequency domain. For pulse or transient signal filtering, a response switch is provided to change the frequency response to the Simple RC mode, optimum for transient-free filtering. Figure 4 shows a comparison of the Filter output response in these modes to a square wave input signal.

CUTOFF RESPONSE

The attenuation characteristics of the Filter are shown in Figure 5. With the response switch in the MAXimally FLAT or Butterworth mode, the gain, as shown by the solid curve, is virtually flat until the -3db cutoff frequency. At approximately two times the cutoff frequency the attenuation rate coincides with the 24 db per octave straight line asymptote. In the Simple RC mode, optimum for transient-free filtering, the dotted line shows that the gain is down approximately 13 db at cutoff and reaches 24 db per octave attenuation rate at five times the cutoff frequency. Beyond this frequency the filter attenuation rate and maximum attenuation, in either mode, are identical.



PHASE RESPONSE

The phase angle at any frequency is the sum of the angles due to the high-pass and low-pass sections of the Filter. Figure 6 gives the phase characteristic for either section in degrees lead (+) or lag (-), as a function of the ratio of the operating frequency f to low cut-off frequency f_L or high-cutoff frequency f_H .

The solid curve is for the maximally flat or Butterworth mode and the dotted curve is for the Simple RC mode.

Example:

Determine the phase shift through the filter, in the maximally flat or Butterworth mode with the low cutoff (f $_{\rm L}$) at 200 Hz, the high cutoff (f $_{\rm H}$) at 600 Hz and an input frequency (f) at 300 Hz.

Phase shift due to low cutoff (f_T)

$$\frac{f}{f_L} = \frac{300}{200} = 1.5$$

from Figure 6 1.5 = $+100^{\circ}$

Phase shift due to high cutoff (f_I)

$$\frac{f}{f_H} = \frac{300}{600} = .5$$

from Figure 6 $.5 = -80^{\circ}$

Total phase shift

$$= +100^{\circ} - 80^{\circ} = +20^{\circ}$$

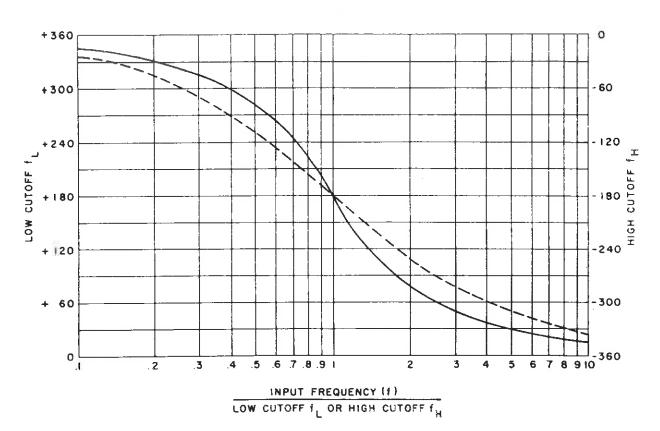


Figure 6. Normalized Phase Characteristics

OPERATION

2.1 INTRODUCTION

On receipt of the Filter, carefully unpack and examine it for damage that may have occurred in transit. If signs of damage are observed, file a claim with the transporting agency immediately, and notify Krohn-Hite Corporation. Do not attempt to use the Filter if damage is suspected.

Rack-mounting models (designated by a suffix "R" after the model number) mount with four machine screws in the standard 19" rack space. No special brackets or attachments are needed.

2.2 FRONT PANEL CONTROLS

The front panel of the Filter includes two frequency dials and associated multiplier switches used to set cutoff frequencies; a power-ON-off switch and indicator light; two BNC coaxial connectors, one for the INPUT signal and one for the OUTPUT signal.

Each frequency dial is calibrated with a single logarithmic scale reading directly in Hz. The dials are 2 1/4 inches in diameter with an effective scale length of approximately 6 inches per band, giving a total effective scale length of approximately 30 inches for the frequency range. The left-hand dial (LOW CUTOFF FREQUENCY) and band multiplier switch select the low cutoff frequency while the right-hand dial (HIGH CUTOFF FREQUENCY) and multiplier switch select the high cutoff frequency.

The LOW CUTOFF FREQUENCY multiplier switch has five positions, covering the frequency range as follows:

Band	Multiplier	Frequency (Hz)
1	1	10 - 100
2	10	100 - 1,000
3	100	1,000 - 10,000
4	1K	10,000 - 100,000
5	10K	100,000 - 1,000,000

The HIGH CUTOFF FREQUENCY multiplier switch has five positions, covering the frequency range as follows:

Band	Multiplier	Frequency (Hz)
1	1	30 - 300
2	10	300 - 3,000
3	100	3,000 - 30,000
4	1,000	30,000 - 300,000
5	10,000	300,000 - 3,000,000

2.3 OPERATION

To operate the Filter, proceed as follows:

- a. Make appropriate power connections as described in Section 2.5.
- b. Make appropriate connections to the IN-PUT and OUTPUT connectors of Filter. The rms voltage should not exceed 3 volts.
- c. Set cutoff frequencies by means of the band multiplier switches (CUTOFF FRE-QUENCY) and the frequency dials. The minimum pass-band is obtained by setting the high cutoff frequency equal to the low cutoff frequency.

d. Turn power switch to ON.

NOTE

The left-hand band multiplier switch and frequency dial are used to select the low cutoff frequency, and the right-hand controls select the high cutoff frequency.

- e. For normal Filter operation the FLOAT-ING/CHASSIS GROUND switch, located on the rear of the chassis, should be in the CHASSIS position. If the Filter is used in a system where ground loops make ungrounded or floating operating essential, this switch should be in the FLOATING position.
- f. When filtering consists principally of separating frequency components of a signal (frequency domain(the RESPONSE switch, located on the rear of the chassis, should be in the MAX-FLAT position. If the Filter is used to separate pulse-type signals from

noise (time domain) this switch should be in the RC position.

2.4 TERMINALS

BNC coaxial connectors are provided on the front panel and on the rear of the chassis for both INPUT and OUTPUT connections.

2.5 LINE VOLTAGE AND FUSES

The Filter, as normally shipped, is connected for operation from an a-c power source of 105-125 volts, 50 to 400 Hz, and uses a 1/8 ampere slow-blow line fuse that is mounted on the rear of the chassis. It may be modified to operate from a 210-250 volt line by removing the two jumpers connecting terminals 1 to 3, and 2 to 4 of the power transformer, and adding a jumper between terminals 2 and 3 of the power transformer. A 1/16 ampere slow-blow fuse should be used for 210-250 volt operation.

CIRCUIT DESCRIPTION

3.1 INTRODUCTION

As shown in the Simplified Schematic Diagram, Figure 2, the Filter consists of an input amplifier for input isolation, a fourpole low-pass filter section (High Cutoff Frequency) with four RC filter networks adjustable by means of a ganged potentiometer assembly and band switch, a four-pole high-pass filter section (Low Cutoff Frequency) with four RC filter networks and a similar ganged potentiometer assembly and band switch. Both cutoff frequencies are tuned capacitively in decade steps by the band switch, and continuously within each decade by the potentiometer assembly.

The Schematic Diagram of the Filter, Figure 8, is attached to the inside rear cover, Bold lines on the Filter schematic show the main signal paths, while the dashed lines indicate feedback signal paths.

3.2 DETAILED DESCRIPTION

INPUT AMPLIFIER

The signal input is capacitor-coupled to the input amplifier, consisting of emitter followers Q201 and Q202, via current limiting resistors R201 and R202, which in conjunction with clamping diodes, CR201 and CR202 prevent damage in the event of excessive input signal. The input amplifier isolates the input and provides the low impedance source necessary to drive the first RC filter network.

LOW-PASS SECTION

The Low-Pass Section consists of a pair of two-pole filters each containing two RC filter networks. Both two-pole filters are adjusted for the proper response to provide a Butterworth characteristic when cascaded.

All RC filter networks are isolated from each other by a buffer amplifier which consists of two emitter followers. The emitter followers, Q205 and Q206, isolate the output of the first two-pole filter from the input of the second two-pole filter. A portion of the output of the first two-pole filter is fed-back via the attenuator consisting of R225 and R227 to obtain the desired response characteristic of the first two-pole filter. An emitter follower, Q207, is used to prevent loading of this attenuator.

The desired response characteristic of the second two-pole filter is effected by feeding back a portion of the output of the second two-pole filter network via the attenuator consisting of R247, R248 and P206. Q212 is an emitter follower to prevent loading of this attenuator. An amplifier consisting of Q210 and Q211 is used to isolate the low-pass section from the high-pass section and also provide the additional gain required on band 5 of the high-pass section.

HIGH-PASS SECTION

The High-Pass Section also consists of a pair of two-pole filters, each adjusted for

the proper response to give a Butterworth characteristic when cascaded. As in the low-pass section emitter followers are used to isolate all the RC filter networks. Q303 and Q304 act as a buffer amplifier between the output of the first two-pole filter and input of the second two-pole filter. This amplifier also provides the gain necessary to compensate for the loss through the filter. The feedback attenuator network consisting of R317 and R318 is used to obtain the desired response characteristic for the first two-pole filter and similarly R326, R327 and P305 modify the response of the second two-pole filter. Q308 and Q309 are buffer followers to provide isolation from the output.

RC/BUTTERWORTH RESPONSE

To provide minimum overshoot to fast rise pulses S202 is used to disconnect the feedback to the second two-pole filters of both the low-pass and high-pass sections.

POWER SUPPLIES

The Power Supplies deliver a plus 10 and minus 10 regulated voltage. It consists of a bridge rectifier CR101 and filter capacitors C101 and C102 to provide the necessary unregulated d-c voltage. The minus 10 volt regulated supply is a typical series type using a zener reference, Z101 and amplifiers Q108 and Q105 which drive a series regulator Q106. To prevent damage when short circuits of the regulated voltage occur, a current limit circuit consisting of Q102 and R103 turns off the minus 10 volt supply if the current in R103 exceeds a predetermined value. The plus 10 volt supply uses the minus 10 volts as a reference. A divider network consisting of R113 and R114 sets the proper voltage level for the amplifiers Q107 and Q104, which drive the series regulator Q103. Q101 and R102 limit the current in the plus 10 volt supply.

MAINTENANCE

4.1 INTRODUCTION

If the Filter is not functioning properly and requires service, the following procedure may facilitate locating the source of trouble. Access to the Filter is accomplished easily by first removing the four screws centered at the rear of each cover. After pulling out the side covers, the top and bottom covers may then be removed.

The general layout of major components, test points, screwdriver controls and adjustments is shown in Figure 7. Detailed component layouts for the three printed circuit cards are included in the Schematic Diagram, Figure 8 which is attached to the inside rear cover. Various check points are shown on the Schematic Diagram and are also marked on the printed circuit cards. To allow for ease of service, PC 302 and PC 303 have been provided with a swing-out mounting. Removal of one screw toward the center of the instrument will allow the card to lift and provide access to the components.

Many troubles may easily be found by visual inspection. When a malfunction is detected, make a quick check of the unit for such things as broken wires, burnt or loose components, or similar conditions which could be a cause of trouble. Any trouble-shooting of the Filter will be greatly simplified if there is an understanding of the operation of the circuit.

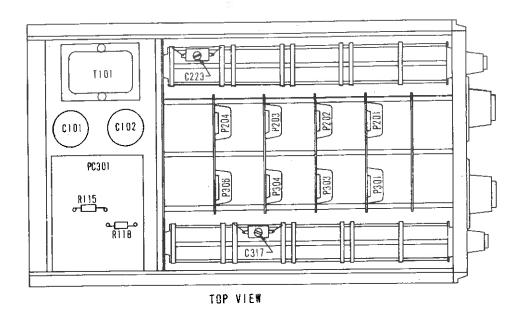
Before any detailed trouble-shooting is attempted, reference should be made to Circuit Description, Section 3, to obtain this understanding.

4.2 POWER SUPPLY

If the Filter does not seem to be working properly, the two power supplies should be checked first. The supplies may be checked most easily at the three terminal barrier strip, located at the bottom rear of the chassis. In general, red leads are tied to the plus 10 volt ±5% supply, while grey leads are tied to the minus 10 volt ±5% supply. If the two supplies appear to be correct, refer to the signal tracing analysis, Section 4.3.

If the minus 10 volt supply is slightly out of tolerance and exceeds its upper limit of minus 10.5 volts, R115 should be increased or R118 should be reduced. When the minus 10 volt supply is slightly below its lower limit of minus 9.5 volts, R115 should be decreased or R118 increased.

If the minus 10 volt supply is correct and the plus 10 volt supply is slightly out of tolerance, R113 or R114 may be defective. A fuse, F101(1/8A for 115v or 1/16A for 230V operation), located at the rear of the instrument, is provided to protect the power supply from short circuits and overloads. The rating of this fuse was selected for proper protection of the instrument, and it should be replaced with one of the same type and rating.



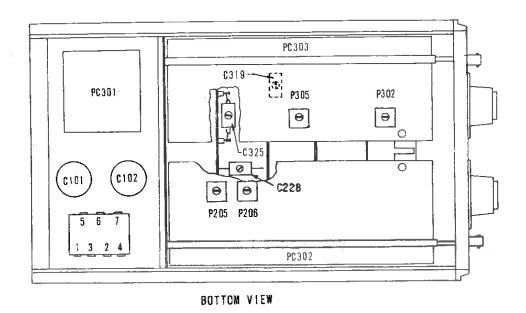


Figure 7. Top and Bottom View of Chassis

Two regulated supplies are used to provide plus 10 volts and minus 10 volts with respect to the chassis. The minus 10 volt supply uses a zener (Z101) as its reference, while the plus 10 volt supply uses the minus supply as its reference. This fact should be kept in mind when doing anywork on the supply, as an error in the minus will be reflected in the plus. Both supplies are provided with current limiting circuits that will shut down the supply when excessive current is being drawn from it. Because of this, an apparent power supply malfunction may be caused by an overload elsewhere in the Filter.

If the supply does not appear to be working properly, the error signal thus developed should be traced through the regulator loop to find the faulty component. Correct voltages for various points in the supply are shown on the Schematic Diagram, Figure 8. As an example of the method of troubleshooting, let us assume that the minus 10 volt supply is very low. This should make the base of Q108 more positive than normal, while making its collector more negative. The base of Q106 should then be made more positive than normal and the collector more negative, thus correcting the output of the supply. If a faulty component is present in the regulating loop this corrective action would be blocked. That component would then be found at the point in the loop where the action was blocked. The plus supply uses approximately the same type of circuit and the same basic method of trouble-shooting may be used there as well.

4.3 SIGNAL TRACING ANALYSIS

If the power supplies appear to be correct but the Filter is not working, the following signal tracing analysis should locate the area of malfunction: Set both the low and high cutoff frequencies to 300 Hz. Connect a 300 Hz 1 volt rms sine wave signal to the input terminals. If the test signal does not appear correctly at the output, the area of the malfunction may be localized by determining where in the Filter the signal first deviates from normal.

Table 1 shows various test points with their correct signal levels. If a test point is found whose signal level differs appreciably from the correct value, the circuitry immediately preceding that test point should be carefully checked.

Table 1.
TEST POINT VOLTAGES

LOW CUTOFF FREQUENCY: HIGH CUTOFF FREQUENCY: RESPONSE SWITCH:	300Hz 300Hz
MAX FLAT	
INPUT: 1 VOLT RMS,	300Hz
SINE WAVE	

SINE V	VAVE	
Card Number	Test Point	Correct Signal Level (rms volts)*
PC 302	27 25 24 23 20 19 18 13 11	1.0 0.9 0.7 0.7 0.5 0.5 0.7 0.7 0.6 0.6
PC 303	23 21 18 16 15 12 10 5 6	0.5 0.5 0.4 0.5 0.7 0.6 0.5 0.5 0.5

 $^{^*}$ Variations of up to $\pm 10\%$ in all readings can be expected,

The test points basically trace the signal through the entire Filter, and they should be checked in the order given.

4.4 TUNING CIRCUITS

If signal tracing shows one of the tuning circuits to be faulty, it should be determined if the trouble is in the resistive or capacitive element. If there is trouble in a capacitive element, this will show up only on a particular multiplier band. If there is a problem in a resistive element, the trouble will be of a general nature and will show up on all multiplier bands.

The values of capacitance used on the two higher bands are selected to compensate for stray capacitance and are therefore not completely in decade ratios of those used on the lower bands. For replacement purposes, a capacitor within $\pm 1\%$ of the specified value can be used with negligible effect on the overall calibration accuracy.

Each of the variable resistance elements consists of four potentiometers ganged together with a gear assembly. Each potentiometer has series and shunt trims to insure proper tracking. The trims and the angular orientation of the potentiometers are carefully adjusted at the factory. If it becomes necessary to change one of these potentiometers, do not attempt to replace the defective potentiometer; instead, notify our Factory Service Department, and they will provide you with the necessary information regarding repair and/or recalibration.

CALIBRATION AND ADJUSTMENT

5.1 INTRODUCTION

The following procedure is provided for the purpose of facilitating the calibration and adjustments of the Filter in the field. The steps outlined follow very closely the operations which are performed on the instrument by our Final Test Department, and strict adherence to this procedure should restore the instrument to its original specifications. It should be noted that some of the tolerances given in this procedure are much tighter than our general specifications. This is to ensure, in test, that all general specifications are met with adequate safety factor. These nominal tolerances, therefore, should not be used for purposes of accepting or rejecting the instrument. If any difficulties are encountered, please refer to Maintenance, Section 4. If any questions arise which are not covered by this procedure, please consult our Factory Service Department.

5.2 DETAILED SPECIFICATIONS

CUTOFF FREQUENCY CALIBRATION

The high and low cutoff frequencies, as defined below, should be within ±5% of the corresponding dial reading. KROHN-HITE Filters are calibrated to conform to passive Filter terminology. The cutoff frequency in the maximally flat or Butterworth mode is the frequency at which the gain of the Filter is 3 db down from the gain at the middle of the pass-band. This pass-band varies with separation of the cutoff frequencies as shown in Figure 3. In the Simple RC or transient-free mode, this cutoff frequency gain is approximately 13 db down.

PASS-BAND GAIN

The Filter output voltage under open circuit conditions will be within \pm 1/2 db of the input voltage for all frequencies within the passband.

To determine the pass-band gain accurately, the high and low cutoff frequencies must be separated by a factor of at least four, and the measuring frequency must be the geometric mean of these frequencies.

ATTENUATION SLOPE

A Typical attenuation curve is shown in Figure 5. At the cutoff frequency, in the maximally flat or Butterworth mode, the slope is approximately 12 db per octave, and at the 12 db point the slope has essentially reached its nominal value of 24 db per octave. The slope of the straight portion of the curve may vary slightly from 24 db per octave at certain frequencies because of cross-coupling effects.

MAXIMUM ATTENUATION

This Filter has a maximum attenuation specification of 80 db which applies over most of the frequency range. At the high frequency end this attenuation is reduced due to unavoidable cross coupling between input and output.

OUTPUT IMPEDANCE

The Filter will operate into any load impedance providing the maximum output voltage and current specification is not exceeded. For a matched load impedance of 50 ohms the insertion loss will be approximately 6 db. Lower values of load resistance will

not damage the instrument but will increase the distortion. Higher values of external load may be used with no sacrifice in performance and correspondingly lower insertion loss. In KROHN-HITE Filters, there is no requirement for the load impedance to match the output impedance.

INTERNALLY GENERATED HUM AND NOISE

The internally generated hum and noise measurement is based on the use of a Ballantine Model 314A Voltmeter, or equivalent. The measurement is made with the input connector shorted, with no other external signal connections to the instrument, and the voltmeter leads shielded.

DISTORTION

Filter distortion is a function of several variables and is difficult to specify exactly. In general, if the Filter is operated within its ratings, distortion products introduced by the Filter and not present in the input signal will not exceed 0.5% of the output signal. In most cases distortion will be considerably less than 0.5%.

5.3 TEST EQUIPMENT REQUIRED

- a. Oscillator capable of supplying at least 3 volts rms from 10 Hz to 10 MHz with frequency calibration better than $\pm 1\%$, distortion less than 0.1% and frequency response within ± 0.2 db. Krohn-Hite Model 4200 or equivalent.
- b. AC VTVM frequency response, 10 Hz to 10 MHz; full scale sensitivity from 1 mv to 10 volts rms with db scale; input capacitance should be less than 20 pf. Ballantine Model 314A or equivalent.
- c. Oscilloscope having direct coupled horizontal and vertical amplifiers with bandwidth of at least 30 MHz and vertical sensitivity of 10 mv per division. Tektronix type 531A or equivalent.

d. High impedance DC voltmeter, capable of measuring 1 millivolt to 15 volts DC.

5.4 POWER SUPPLIES

With the Filter operating at 115 or 230 volts line, whichever is applicable, check the plus and minus 10 volt supplies with respect to chassis ground. The Floating / Chassis grounding switch, located at the rear of the chassis, should be in the Chassis position. The supplies may be checked most easily at the three terminal barrier strip, located at the bottom rear of the chassis. In general, red leads are used for the plus 10 volt ±5% supply, while grey leads are used for the minus 10 volt ±5% supply. If the minus 10 volt supply is slightly out of tolerance and exceeds its upper limit of minus 10.5 volts, R115 should be increased or R118 should be reduced. When the minus 10 volt supply is slightly below its lower limit of minus 9.5 volts, R115 should be decreased or R118 increased.

5.5 DETAILED TEST PROCEDURE

Table 2 contains detailed test procedures to check the Filter performance. The procedures are to be performed in the given order (1 through 18). Throughout the procedures, low cutoff is abbreviated LCO and high cutoff is abbreviated HCO. Note that low cutoff dial and multiplier refers to the left-hand frequency dial and band multiplier switch, and that high cutoff dial and multiplier refers to the right-hand frequency dial and band multiplier switch. For all steps, the AC input line voltage should be at 115 or 230 volts, whichever is applicable.

The general layout of major components, test points, screwdriver controls and adjustments is shown in Figure 7. To obtain

access to the trim capacitors C228, C319 and C325, it is necessary to remove the screws that secure the large hinged printed circuit cards.

In the event the Filter does not meet the correct tolerance as specified in each step of the detailed test procedure, reference should be made to Section 4, Maintenance.

NOT FOR 3103(R)-4

TABLE 2. DETAILED TEST PROCEDURE

-2406

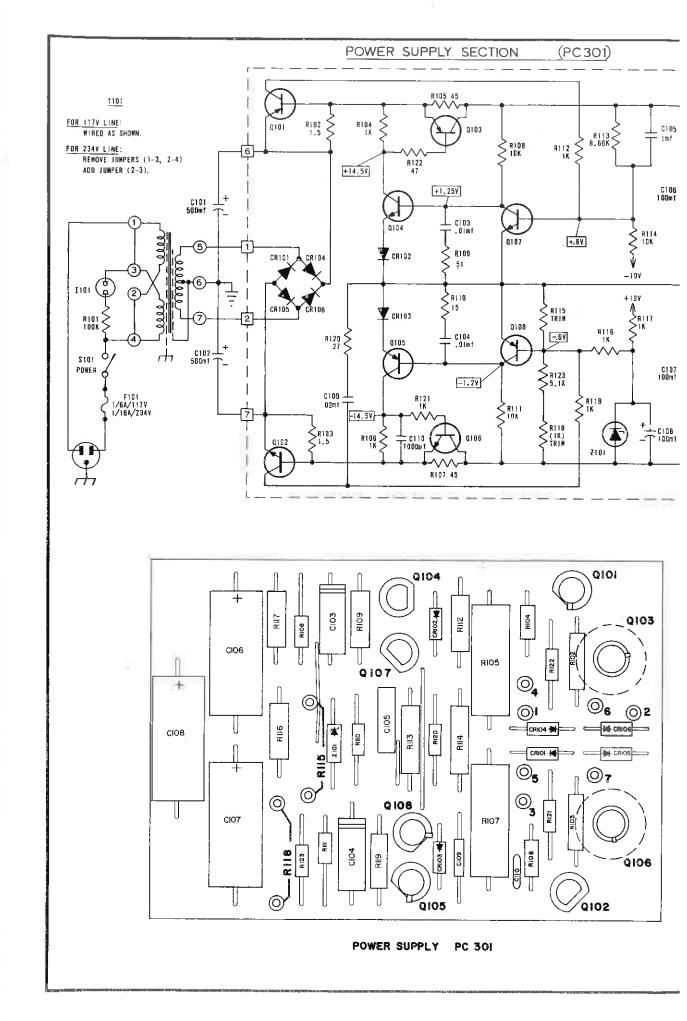
			FREQUENC	Y SETT	ING	INPL	JT SIGNAL			
STEP	PROCEDURE	LCO Dial	LCO Multiplier	HCO Dial	HCO Multiplier	VOLTS (RMS)	Frequenc			
1.	LCO dial calibration at 30	30	X10	300	X10K	0.5	300Hz			
	Connect scope vertical input to Filter output. Connect scope horizontal input and oscillator to Filter input. Set response switch (rear of chassis) to max flat position. Adjust LCO dial to close the ellipse at about a 135 degree angle. If necessary, loosen LCO dial screws and set dial to 30.									
2.	LCO dial gain calibration at 30	30	X10	300	X10K	0.5	300Hz			
	Switch LCO frequency multiplier to X1 position. Connect AC VTVM to Filter output. Adjust oscillator output until VTVM indicates exactly 14 db. Return LCO frequency multiplier to X10 position. Adjust P305 until VTVM indicates 11 db. If P305 requires adjustment, recheck 14 db reference level.									
3.	LCO dial gain calibration at 10	10	X10	3 0 0	X10K	0.5	100 Hz			
	Switch LCO frequency multiplier to 2 indicates exactly 14 db. Return LCC LCO dial until VTVM indicates 11 db	J [reai	leney muli	tinlian	to V10 no	aition A	-1			
4.	LCO dial gain calibration at 100	100	X10	300	X10K	0.5	1KHz			
	Switch LCO frequency multiplier to X1 position. Adjust oscillator output until VTVM indicates exactly 14 db. Return LCO frequency multiplier to X10 position. Adjust LCO dial until VTVM indicates 11 db. Tolerance is a dial setting from 95 to 105.									
					-0		105.			
5.	Unity gain adjustment at 5kHz.	70	X1	45	X10K	1.0	5kHz			
5.		70	X1	45	X10K	1.0				
5. 6.	Unity gain adjustment at 5kHz. With VTVM, compare AC signal on i adjust P302 for unity gain. X10K band calibration	70 nput F	X1 Pilter with	45 AC si	X10K gnal on ou	1.0 Itput. If n	5kHz necessary,			
	Unity gain adjustment at 5kHz. With VTVM, compare AC signal on it adjust P302 for unity gain.	70 nput F	X1 Pilter with X100	45 AC si	X10K gnal on ou	1.0 Itput. If n	5kHz necessary,			
6.	Unity gain adjustment at 5kHz. With VTVM, compare AC signal on it adjust P302 for unity gain. X10K band calibration Switch LCO multiplier to X10K positi 0.3 db) in output amplitude when switt position. Change input frequency to 50 kHz, sw oscillator amplitude until VTVM indices Filter. Switch LCO multiplier to X10K	70 nput F 10 on, A ching ritch I cates of the position of the	X1 Cilter with X100 Adjust P20 LCO multipexactly 0.	300 5 for riplier olier to	X10K gnal on ou X10K ninimum from X100 X100 poo , 20 db oo	1.0 atput. If no o.5 change (lee o position. Acomp output of	5kHz necessary, 1MHz ess than to X10K			
6, [a, b, c,	Unity gain adjustment at 5kHz. With VTVM, compare AC signal on it adjust P302 for unity gain. X10K band calibration Switch LCO multiplier to X10K positi 0.3 db) in output amplitude when swit position. Change input frequency to 50 kHz, sw oscillator amplitude until VTVM indices.	70 nput F 10 on. A ching ritch I cates of the cates of t	X1 Cilter with X100 Adjust P20 LCO multipexactly 0. Sition. If is down 2. LCO multipexactly 0. Sition. Addition. Addition. Addition. Addition.	300 5 for riplier colier to 1 volts necess 4 db ar iplier i 1 volts just L0 colier to	X10K gnal on ou X10K X10K ninimum from X100 0 X100 poor ary, adju ad repeat to X1K poor 1, 20 db ou CO dial un 5 If off	1.0 ttput. If n 0.5 change (le 0 position sition. Ac n output of st C317 ar part a. osition, An output of n output of	5kHz necessary, 1MHz ess than to X10K djust f nd Adjust f			

TABLE 2. DETAILED TEST PROCEDURE (Cont.)

			FREQUENCY	SETT	ING	INPL	IT SIGNAL				
STEP	PROCEDURE	LCO Dial	LCO Multiplier	HC0 Dial	HCO Multiplier	VOLTS (RMS)	Frequency				
1	X1K position. Adjust of cillafor amy 0.1 volts, 20 db on output of Filter. •Adjust C325 until VTVM indicates 17	Swite db.	e until VT ch LCO mu	VM ind Iltiplie	licates ex r to X10K	actly Cposition.					
e.	Set LCO dial to 30. Set input frequer position. Adjust oscillator amplitude of Filter. Set LCO multiplier to X10 indicates 17 db. Tolerance is a dial tolerance, divide the error between 1	e unti. K pos settir	ition. Ad gition. Ad ng from 28	dicate just L .5 to 3	s exactly CO dial u 81.5. If c	20 db on c ntil VTVN	output				
7.	LCO dial gain calibration at 30 on all bands										
a.	X1 Calibration	30	X1	300	X10K	0.1	As noted				
	output until VTVM indicates exactly 2	20 db.	lator frequ Change f ce is a dia	reque	acy to 30	Hz. Adju	st LCO				
b,	X100 Calibration	30	X10	300	X10K	0.1	3kHz				
	Adjust oscillator output until VTVM i multiplier to X100 position. Adjust I is a dial setting from 28.5 to 31.5.										
c.	X1K Calibration	30	X100	100	X10K	0.1	30kHz				
•	Adjust oscillator output until VTVM i multiplier to X1K position. Adjust L is a dial setting from 28.5 to 31.5.	ndica CO di	tes exactly ial until V	720 dk ΓVM ii	o. Set LC ndicates 1	O frequen 7 db. To	lcy lerance				
8,	HCO dial calibration at 90	90	X10	90	X10K	0.5	900Hz				
	Connect oscillator output to scope horizontal input; adjust scope for horizontal deflection of 20 divisions. Remove oscillator output from scope horizontal input and connect to scope vertical input; adjust scope for vertical deflection of 20 divisions. Remove oscillator output from scope and connect to Filter input. Connect scope horizontal input to input of Filter and scope vertical input to Filter output. Adjust LCO dial to close ellipse at about a 45 degree angle. Switch HCO multiplier to X10 position. Adjust HCO dial to close ellipse at about a 135 degree angle. If necessary, loosen HCO dial screws and set dial to 90.										
9.	HCO dial gain calibration at 90	10	X1	90	X10	0.5	900Hz				
	Switch HCO frequency multiplier to X100 position and adjust oscillator output until VTVM indicates exactly 14 db. Return HCO frequency multiplier to X10 position. Adjust P206 until VTVM indicates 11 db.										
10.	HCO dial gain calibration at 30	10	X1	30	X10	0.5	300Hz				
	Switch HCO frequency multiplier to X VTVM indicates exactly 14 db. Return Adjust HCO dial until VTVM indicates 28.5 to 31.5.	rn HČ	O frequen	ey mul	tiplier to	X10 posit	ion.				
11.	HCO dial gain calibration at 300	10	X1	300	X10	0.5	3 KHz				
	Switch HCO frequency multiplier to X indicates exactly 14 db. Return HCO HCO dial until VTVM indicates 11 db.	frequ	osition and lency mult	iplier	to X10 po	sition. A	djust				

TABLE 2. DETAILED TEST PROCEDURE (Cont.)

		FREQUENCY SETTING									
		LCO	LCO	нсо		VOLTS	T SIGNAL				
STEP	PROCEDURE	Dial	Multiplier	Dial	Multiplier	(RMS)	Frequency				
12.	X10K band calibration		X1	30	X10K	0.1	30 kHz				
	Adjust oscillator output until VTVM indicates exactly 20 db. Change oscillator frequency to 300 KHz. Adjust C223 until VTVM indicates 17 db. Set filter dial to 300 and oscillator to 3 MHz. Adjust C228 until VTVM indicates 17 db. Check 90 on the dial with the oscillator set at 90 kHz. (It may be necessary to divide the error by readjusting C223 and C228.)										
13.	HCO dial gain calibration at 100 on all bands										
а.	X1K band calibration	10	X1	100	X10K	0.1	100kHz				
	Adjust oscillator output until VTVM to X1K position. Adjust HCO dial ur setting from 95 to 105.	indica itil VT	tes exactl VM indic	y 20 d ates 17	b. Switch 7 db. Tole	HCO mul erance is	+inlian				
b.	X100 band calibration	10	X1	100	X1K	0.1	10kHz				
	Adjust oscillator output until VTVM to X100 position. Adjust HCO dial u setting from 95 to 105.	indica ntil V	tes exactl	y 20 di cates 1	o. Switch 7 db. Tol	HCO mul erance is	tiplier a dial				
c, [X1 band calibration	10	X1	100	X10	0.1	100Hz				
	Adjust oscillator output until VTVM X1 position. Adjust HCO dial until V from 95 to 105.	indica: TVM	tes exactl indicates	y 20db 17 db.	. Switch I Tolerand	HCO mult ce is a dia	iplier to al setting				
14.	Maximum attenuation at 90 KHz	100	X10K	30	X10K	3.0	90kHz				
	Output signal should be below 330 mi	crovol	ts.								
15.	Maximum attenuation at 3MHz	10	X10K	30	X10K	3.0	3 MHz				
	Output signal should be below 3.3 mi	llivolt	s.		111011	0.0	3141112				
16.	Maximum input voltage	100	X1	300	X10K	3.0	300kHz				
_	Check that output signal is not distor	ted.					300K112				
17.	Output impedance	100	X1	300	X10K	1.0	1kHz				
	Connect 50 ohm resistor to Filter ou approximately 0.5 volts. Remove 50	tput.	Output si	- 1			TRIIZ				
18.	Hum and Noise	10	X1	300	X10K	0					
	Remove Oscillator, Connect VTVM across the input connector. Replace 150 microvolts. Caution! If output le output to be sure excessive output is ference.	all co evel is	Filter ou	utput a	nd a shorti gnal level	ing jumpe should be	below				

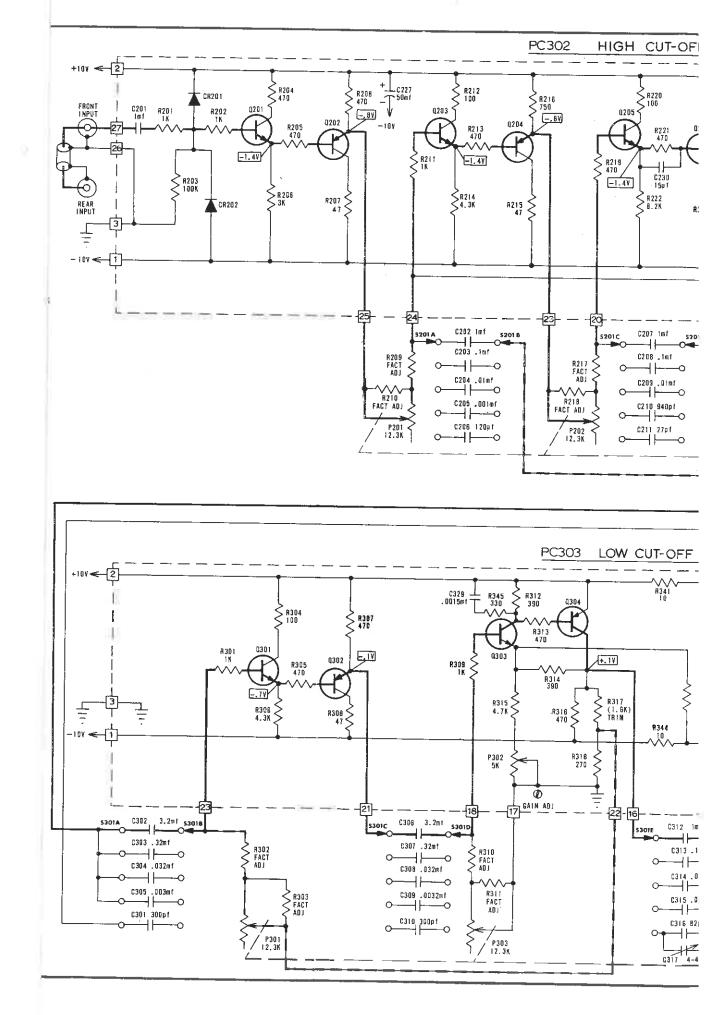


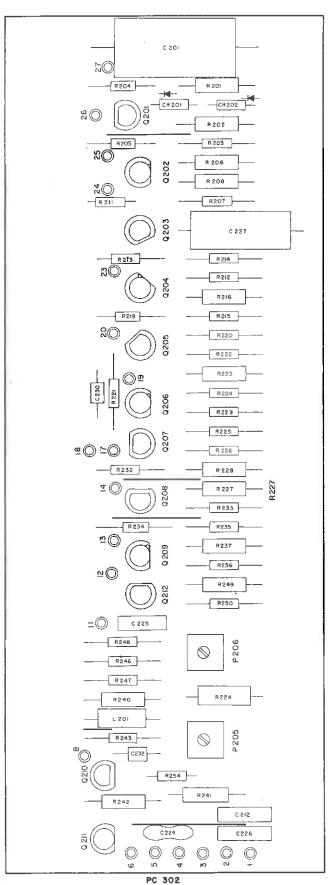
					RES	SIST	ORS					
Symbol	De	scription		Mfr.	Part No.		Symbol	Desc	ription		Mfr.	Part No.
R101 R102 R103 R104 R105 R106 R107 R108 R109 R110 R1112 R112 R113 R114 R115 R116 R117	100K 1.5 1.5 1K 45 1K 45 10K 51 15 10K 1K 8.66K 10K TRIM 1K 1K	10% 3% 3% 5% 3% 5% 5% 5% 10% 5% 10% 1% 1%	1/4W 1W 1W 1W 1/4W 5W 1/4W 5W 1/4W 1/2W 1/4W 1/4W 1/4W 1/4W 1/4W 1/4W 1/2W	AB NYT AB NYT AB NYT AB NYT AB	CB1041 1000S 1000S 1000S CB1025 1500S CB1025 1500S CB1025 1500S CB1035 CB1035 CB1031 CB1035 CB1021 M4-T1-8.66K M3-T1-10K TYPE CB EB1025 EB1021 TYPE CB		R238 R239 R240 R241 R242 R244 R244 R246 R247 R248 R249 R250 R251 R252 R253 R254	TRIM TRIM 1K 510 470 220 270 470 910 1.2K 1K 100 47 1 BK 27	10% 5% 20% 10% 5% 20% 5% 10% 10% 20% 10% 20%	1/2W 1/4W 1/4W 1W 1/4W 1/4W 1/4W 1/4W 1/4W	AB AB AB AB AB AB AB AB AB AB AB	TYPE CB TYPE CB EB1021 EB5115 CB4712 CB2211 GB2715 CB4712 CB9115 CB1221 EB1025 CB1012 CB4702 CB1022 CB1022 CB1022
R119 R120 R121 R122 R123	1K 27 1K 270 5.1K	10% 10% 10% 10% 5%	1/2W 1/4W 1/2W 1/4W 1/4W	AB AB AB AB AB	EB1021 CB2701 EB1021 CB2711 CB5125 EB1021		R302 R303 R304 R305 R306 R307 R308	TRIM TRIM 100 470 4.3K 470 47	20% 20% 5% 5% 10%	1/4W 1/4W 1/4W 1/2W	AB AB AB AB AB AB	TYPE CB TYPE CB CB1012 CB4712 CB4325 EB4715 CB4701
R202 R203 R204 R205 R206 R207 R208 R209 R210	1K 100K 470 470 3K 47 470 TRIM TRIM 1K	10% 10% 20% 20% 5% 10% 5%	1/2W 1/4W 1/4W 1/4W 1/2W 1/4W 1/2W	AB AB AB AB AB AB AB AB	EB1021 CB1041 CB4712 CB4712 EB3025 CB4701 EB4715 TYPE CB TYPE CB		R309 R310 R311 R312 R313 R314 R315 R316 R317 R318	1K TRIM TRIM 390 470 390 4.7K 470 1.6K 270	10% 20% 10% 10% 5% 5% 5%	1/4W 1/4W 1/4W 1/4W 1/2W 1/2W 1/2W	AB AB AB AB AB AB AB AB	CB1022 TYPE CB TYPE CB CB3911 CB4712 CB3811 CB4721 EB4715 CB1625 EB2715
R211 R212 R213 R214 R215 R216 R217 R218 R219 R220	100 470 4.3K 47 - 750 TRIM TRIM 470 100	20% 20% 5% 10% 5% 20%	1/4W 1/4W 1/4W 1/4W 1/2W 1/4W	AB AB AB AB AB AB AB AB	CB1012 CB4712 CB4325 EB4702 EB7515 TYPE CB TYPE CB CB4712 CB1012		R319 R320 R321 R322 R323 R324 R325 R327 R328	3.9K 1K 100 470 4.3K TRIM TRIM 620 1K	5% 20% 20% 20% 5% 5%	1/4W 1/4W 1/4W 1/4W 1/4W	AB AB AB AB AB AB AB AB	CB3925 CB1022 CB1012 CB4712 CB4325 TYPE CB TYPE CB EB6215 CB1022
R221 R222 R223 R224 R225 R226 R227 R228 R229 R230	470 8.2K 1.5K 47 5.1K 470 1K 820 100 TRIM	20% 5% 5% 10% 5% 20% 5% 20% 5%	1/4W 1/4W 1/2W 1/4W 1/4W 1/4W 1/2W 1/2W	AB AB AB AB AB AB AB AB	CB4712 CB8225 EB1525 CB4702 CB5125 CB4712 EB1025 EB8215 CB1012 TYPE CB		R329 R330 R331 R332 R333 R334 R335 R336 R336 R337 R338	47 430 47 4.3M 100 1K 470 4.3K TRIM TRIM	10% 5% 10% 5% 20% 20% 5%	1/4W 1/2W 1/4W 1/4W 1/4W 1/4W 1/4W	AB AB AB AB AB AB AB AB	CB4702 EB4315 CB4702 CB4355 CB1012 EB1022 CB4712 CB4325 TYPE CB TYPE CB EB4715
R231 R232 R233 R234 R235 R236 R237	TRIM 100 100 100 4.3K 47 470	20% 20% 20% 5% 10% 5%	1/4W 1/4W 1/4W 1/4W 1/4W	AB AB AB AB AB AB	CB1012 CB1012 CB1012 CB1012 CB4325 CB4702 EB4715		R339 R340 R341 R342 R343 R344 R345	470 47 10 51 10K 100 330	5% 10% 5% 10% 20% 10%	1/2W 1/4W 1/4W 1/2W 1/4W 1/4W	AB AB AB AB AB	CB4715 CB4702 CB1001 EB5105 CB1031 CB1012 CB3311

MANUFACTURERS CODE								
AB ASP CD CK BKM CW DLV ELM ERT GE KH	(01121) (82142) (06751) (09353) (30646) (79727) (99800) (72136) (72982) (03508) (88865)	Allen Bradley Co. Airco Speer Cornell-Dubilier Components, Inc. CAK Components Reckman Instr. Co. Continental Wirt Elec. Delevan Electronics Electromotive Mfg. Erie Technological General Electric Krohn-Hite	Milwaukee, Wisc. Dubois, Pa. Mewark, M.J. Biddeford, Me. Watertown, Mass. Cedar Grove, N.J. Philadelphia, Pa. East Aurora, N.Y. Willimantic, Conn. Erie, Pa. Syracuse, N.Y. Cambridge, Mass.	MAL MOT MSC NYT SIL SP STT SWC TI TL TR TRW	(04713) (14552) (17856) (56289) (82389) (01295) (94322) (03877) (84411)	P.R. Mallory & Co. Motorola Semiconductor Micro Semiconductor Corp. Nytronics Siliconix Sprague Electric CO. Stettner-Trush Switchcraft Inc. Texas Instruments, Inc. Tel Labs Transitron Electric Co. TRW Corp.	Indianapolis, Ind. Phoenix, Ariz. Culver City, Calif. Darlington, SC. Sunnyvale, Calif. North Adams, Ma. Cazanovia, N.Y. Chicago, Ill. Dallas, Texas Manchester, N.H. Wakefield, Mass. Ogallala, Neb.	

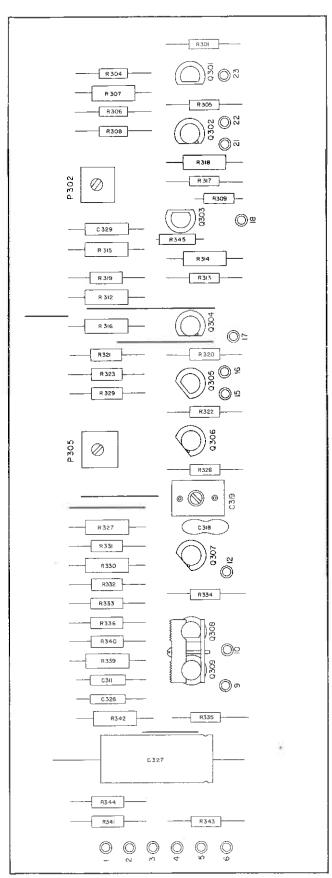
S ymbol	
C101 C102 C103 C104 C105 C106 C107 C108 C109 C110	500 500 .0 .0 .0 100 100 .01
C201 C202 C203 C204 C205 C206 C206 C207 C208 C209 C210 C211 C212 C213 C214 C215 C216 C218 C219 C220 C221 C223 C224 C225 C226	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

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PC 302
HIGH CUTOFF FREQUENCY
(low pass section)



Symbol 5 | R101 R102 R103 R104 R105 R107 R108 R109 R110 R112 R113 R114 R115 R117 R118 R119 R120 R122 R123 R227 R228 R229 R230 R231 R232 R233 R234 R235 R236 R237

AB ASP	(011 (821
DD DT DK	(067 (093
BKM CN! DLV	(396 (797 (998
ELM ERT GE	(721 (729 (035
КН	388)

PC 303 LOW CUTOFF FREQUENCY (high pass section)

MODIFICATION SHEET

MODEL NO. 3103

SCHEMATIC DATE 10-22-73

DATE 4-4-74

Serial Nos.

545,549,553,555,561, 563,565,566,569-up

814-up

Change and/or Modification

C225 has been changed from 89pf, 1% type CM to 62pf, 5% type CM.

C206 has been changed from 12pf, 5% type DM to 82pf, 5% type CM.

R225, 15K, 10%, $\frac{1}{4}$ W has been added in series with C211.

R339 has been changed from 470 ohm, $\frac{1}{2}$ W, 5% to 390 ohm, $\frac{1}{2}$ W, 5%.

MODIFICATION SHEET

MODEL NO. 3103

SCHEMATIC DATE

DATE 2-25-77

Serial Nos.

Documentation: Manual Dated 1973.

Change and/or Modification

1. Section 1.2, Page 2, Specifications, Cutoff frequency calibration accuracy should read:

"±5% (± 10% on band 5) with RESPONSE switch in MAX FLAT .."

Section 5.2, Page 13, Detailed Specifications, Paragraph 1, Line 2 should read:

". . . fined below, should be within ±5% (±10% on band 5) of the . . ."

3. Table 2, Page 16, Step 8, Line 6, should read:

"... LCO dial to close ellipse at about a 135 degree angle.
Switch HCO multiplier to X10

4. Table 2, Page 16, Step 8, Line 8 should read:

". . . position. Adjust HCO dial to close ellipse at about a 45 degree angle. If necessary . . "

Documentation: Manual Dated 1973

The 19" rack-mounting version of the Model 3103, designated 3103R has been discontinued. Starting with Serial No. 874 an optional rack-mounting kit, Part No. RK-38, was made available to convert the standard bench model for 19" rack-mounting.



Avon Industrial Park / Bodwell St., Avon, Mass. 02322 U.S.A. Telephone 617/580-1660 — TWX 710-345-0831